

# Modeling of Wall-boiling Phenomena from Nucleate Subcooled Boiling up to CHF Conditions

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#### Outline

- The NUBEKS R&D consortium (2014-2018)
- What is Critical Heat Flux (CHF)?
- Model formulation for CFD simulation of CHF
  - Extended RPI model  $\Leftrightarrow$  Inhomogeneous MUSIG  $\Leftrightarrow$  CHT
- The KIT COSMOS-L test facility
  - The test matrix
  - Wall boiling & CHF simulations
- Concluding remarks and outlook



### The NUBEKS R&D Consortium

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 R&D Consortium (July 2014 – June 2018): "CFD Methods for the Prediction of Critical Heat Flux" NUBEKS – Numerische Beschreibung Kritischer Siedevorgänge



# What is Critical Heat Flux (CHF)?

- Critical Heat Flux (CHF):
  - Sometimes referred to as the boiling crisis or departure from nucleate boiling (DNB)
  - With increased wall heat flux, suddenly the heat transfer at a heater surface becomes inefficient.
    - → Applied heat can no longer be removed from the heater surface by so far acting heat transfer mechanisms, i.e. mainly by evaporation/boiling
       → Sudden excursion of wall temperature

    - $\rightarrow$  Can lead up to destruction of the heater material (melting)
- CHF mechanisms / explanations:
  - Near wall vapor bubble crowding
  - Vapor film @ wall is shielding the heater wall from subcooled liquid
  - Sublayer dryout, i.e. liquid film underneath vapor layers close to heater wall are drying out  $\Rightarrow$  dry patch formation

CHF at upper end of heater rod in COSMOS-L, Image by courtesy of Florian Kaiser, KIT / IKET

# Model Formulation for CFD Simulation of CHF - Extended RPI Wall Boiling Model -

- The extended RPI Wall Boiling Model accounts in addition for the convection to the vapor phase
- Heat flux partitioning:

$$Q_W = f(\alpha_l) \cdot \left(Q_c + Q_q + Q_e\right) + \left(1 - f(\alpha_l)\right) \cdot Q_g$$

- *Q<sub>c</sub>* : single phase convection to liquid
   *Q<sub>e</sub>* : evaporation
- $Q_q$  : quenching
- $Q_g$  : single phase convection to gas





# Model Formulation for CFD Simulation of CHF The MUSIG Model

- MUSIG = Multiple Size Group Model
  - Discrete Population Balance Model for poly-dispersed flows
  - Particle size distribution is discretized by assigning bubbles to different 'size groups'
- Homogeneous MUSIG
  - Assumes single velocity field for all bubble classes (one dispersed phase)
  - Valid for bubbly flows in spherical / elliptic regime and when lift force can be neglected
- Inhomogeneous MUSIG
  - Allows multiple velocity fields for groups of bubble classes (more than one dispersed phase, i.e. more than 1 set of N.-S. eq.'s)
  - Several bubble size classes can belong to the same 'velocity group'
  - Useful when different bubble size classes have very different velocity fields, e.g. due to change of sign of the lift force.
    - Allows for separation of bubbles of different diameter based on acting forces and governing physics



# Model Formulation for CFD Simulation of CHF MUSIG + Interphase Mass Transfer



# Model Formulation for CFD Simulation of CHF MUSIG + Wall Boiling



### CFD Setup Characteristics – iMUSIG

Extended RPI wall boiling model ⇔ Inhomogeneous MUSIG ⇔ CHT					
Version	18.1 + Customized Solver				
Analysis Type	Steady runs with fluid time scale $\Delta t$ = 0.005 [s]				
Material Properties	IAPWS IF-97 Library				
Interfacial forces	Lift	Tomiyama			
	Drag	Grace			
	Turbulent Dispersion	FAD turbulent dispersion model			
Boiling Model	Equilibrium RPI model	Maximum Area Fraction of Bubble Influence = 10			
	Bubble Departure Diameter	Tolubin	Folubinski et al. (default)		
	Nucleation Site Density	Lemmert et al.(default) / Modified Reference Site Density			
Vapor heat transfer	Thermal Energy				
Turbulence model	SST		Homogeneous Turbulence		
IMUSIG	Breakup Coeff. = 1.0 ; Turb. Coalescence Coefficient = 10.0				
	Boundary Conditions: Size Fraction of the smallest group = 1 @ Domain Openings and Domain Initialization				
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# The COSMOS-L Test Facility (KIT/IKET)



# The COSMOS-L Test Facility (KIT)

Experiments by KIT / TVT and KIT / IKET :

- Prof. Dr. Thomas Wetzel
- Dr. Stephan Gabriel
- Florian Kaiser
- Wilson Heiler

#### **Reference:**

Christoph Haas: "Critical Heat Flux for Flow Boiling of Water at Low Pressure on Smooth and Micro-Structured Zircaloy Tube Surfaces", KIT Scientific Publishing, Karlsruhe, 2012.



Images by courtesy of St. Gabriel & F. Kaiser (KIT)





# The COSMOS-L Test Facility (KIT)

- Axially symmetric
  - Heat Flux prescribed on the inner ZircAlloy heater rod surface
- Radial dimensions
  - Inner radius of Zircaloy-Tube:  $R_{ic} = 4.18 \text{ mm}$
  - Outer radius of Zircaloy-Tube : R<sub>ac</sub> =4.75 mm
  - Inner radius of Duran-Domain: R<sub>id</sub> = 9 mm
  - Outer radius of Duran-Domain :  $R_{ad} = 10.9 \text{ mm}$
  - Annulus (Water-Domain) width : 4.25 mm
- Axial dimensions
  - Total heating section height:  $L_{Heated}$  = 326 mm



# The COSMOS-L Test Facility (KIT) The Test Matrix

- T80P1200M400
   Operating Conditions
  - Liquid SubCooling: 20 [K]
     i.e. Water Inlet Temperature: 80°C
  - Reference Pressure: 1.2 [bar]
  - Mass Flux : 400 [kg/m<sup>2</sup>s]



- Calculating boiling curves starting from 400 [kW/m<sup>2</sup>] Heat Flux
- Further investigated operating conditions:
  - T80P2000M400 pressure variation
  - T80P2000M600 add. mass flux variation
  - T65P1200M400 liquid subcooling variation

### **COSMOS-L:** Material Parameters

• Water / Water Vapor : from IAPWS material library

Material	IAPWS IF97
Minimum Temperature	50 [C]
Maximum Temperature	400 [C]
Minimum Absolute Pressure	0.8 [bar]
Maximum Absolute Pressure	2 [bar]
Number of Points	600

- ZircAlloy-4 : CES Edupack 2010 material data sheet
- Duran glass outer walls : manufacturer material data sheet http://www.duran-group.com/de/ueber-duran/duran-eigenschaften.html)

# **COSMOS-L:** Polydispersed Fluid Resolution

- Two velocity groups with 26 size classes equidistantly distributed within each velocity groups
  - 20 size groups for the first velocity group
    - Minimum diameter: 0.02 [mm]
    - The smallest observable bubble diameter been estimated by means of the provided HD videos to be around 0.1-0.2 [mm]
    - Bubble Departure Diameter (Lift-Off) according to Tolubinski et al. is approx. 0.4 mm
  - 6 size groups for the second velocity group
    - Maximum diameter: 7 mm
  - Minimum Volume Fraction = 1E-9
- Transition diameter is the diameter where the Tomiyama Lift coefficient changes sign: 5.33339 [mm] @ 1.2 [bar] & 377.93 [K]



#### T80P1200M400

(Reference Case)



# The COSMOS-L Test Facility (KIT) T80P1200M400: CHF at Q<sub>wall</sub> = 850 [kW/m<sup>2</sup>]

- Cladding temperature excursion (mean domain temperatures are monitored)
- Previous simulation runs show restarts from:

$$Q_{wall} = 400 [kW/m^{2}]$$
  

$$\Rightarrow Q_{wall} = 550 [kW/m^{2}]$$
  

$$\Rightarrow Q_{wall} = 700 [kW/m^{2}]$$
  

$$\Rightarrow Q_{wall} = 850 [kW/m^{2}]$$

 Q<sub>wall</sub> = 800 [kW/m<sup>2</sup>] does not yet show this strong cladding temperature increase but behaves like the 700-er case with T<sub>wall</sub>~408.2 [K]

 $\rightarrow$  mean T<sub>wall</sub> increase by ~50 [K]



### The COSMOS-L Test Facility (KIT) T80P1200M400: The Boiling Curve



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# The COSMOS-L Test Facility (KIT) Reference Case T80P1200M400

- The experimentally measured heat flux at which CHF occurs is about 867 [kW/m<sup>2</sup>] with a standard deviation equal to 16 [kW/m<sup>2</sup>]
- This is in good agreement with the ANSYS CFX results
  - Temperature excursion in the ZircAlloy heater rod obtained @ 850 [kW/m<sup>2</sup>] in the simulations
  - Liquid cooling of ZircAlloy cladding breaks down at the very end of the heater rod



# CHF at $Q_{wall} = 850 [kW/m^2]$

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• CHF in the ZircAlloy cladding and highly superheated steam in both MUSIG velocity groups showing almost the same temperature



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### Temperature Distribution with Increased Wall Heat Flux : 600 [kW/m<sup>2</sup>] $\rightarrow$ 850 [kW/m<sup>2</sup>]





#### T80P2000M400

#### (Reference Pressure Variation)



#### The COSMOS-L Test Facility (KIT) T80P2000M400 Boiling Curve – Size Classes



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# The COSMOS-L Test Facility (KIT) T80P2000M400 Boiling Curve – Avg./Max. T<sub>Wall</sub>



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# The COSMOS-L Test Facility (KIT) T80P2000M400 - CHF Comparison

- The experimentaly measured heat flux at which CHF occurs is about 1229 [kW/m<sup>2</sup>] with a standard deviation equal to 9 [kW/m<sup>2</sup>]
- This is in good agreement with the ANSYS CFX results
  - Temperature excursion in the Zircalloy heater rod obtained @ approx. 1300 [kW/m<sup>2</sup>] in the simulations
  - Liquid cooling of ZircAlloy cladding breaks down at the very end of the heater rod



T80P2000M400 @ 1360 [kW/m2]

#### T80P2000M400: Temperature Distribution





#### T80P2000M600

(Reference Pressure and Fluid Mass Flow Rate Variation)



# The COSMOS-L Test Facility (KIT) T80P2000M600 Boiling Curve – Avg./Max. T<sub>Wall</sub>



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#### T80P2000M600: Temperature Distribution





#### T65P1200M400

#### (Fluid Subcooling Temperature Variation)



# The COSMOS-L Test Facility (KIT) T65P1200M400 Boiling Curve – Avg./Max. T<sub>Wall</sub>



#### T65P1200M400 Temperature Distribution

- Due to the thinned vapor layer at the wall this case required the increase of the resolution of the number of classes for the velocity group of large bubbles from 3 to 6
- Maximum wall temperature is reached as in all other cases towards the outlet of the annular test section of COSMOS-L
- The wall and vapor temperature excursion was finally predicted for applied wall heat fluxes beyond 1255 [kW/m<sup>2</sup>]



T65P1200M400\_H1255





# Concluding Remarks and Outlook

- Presented a short overview of the NUBEKS R&D project results obtained by ANSYS Germany for CFD modeling and simulation of Critical Heat Flux (CHF)
- Successfully predicted the boiling curve up to CHF for 4 experimental series from COSMOS-L (KIT) test facility

 $\Rightarrow$  CHF detection by temperature excursion in the heater CHT domain

- Key ingredients:
  - ANSYS CFX 18.0 or newer
  - CHT for the heater material
  - Extended RPI wall boiling model
  - Inhomogeneous MUSIG model for the vapor phase IAD
- Some challenges and modeling uncertainties remain:
  - Nucleation site density specification
  - Break-up and coalescence modeling
  - Flow regime transition ⇔ Multiphase flow turbulence modeling
  - Extraordinary thin vapor layers at high liquid subcooling / high liquid mass flux



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